



## A multi-isotope model for simulating soil organic carbon cycling on an eroding landscape (WATEM\_C v1.0)

Zhengang Wang<sup>1,2</sup>, Kristof Van Oost<sup>2</sup>

<sup>1</sup>Guangdong Provincial Key Laboratory of Urbanization and Geo-simulation, School of geography and  
5 planning, Sun Yat-Sen University, Guangzhou 510275, China

<sup>2</sup>Georges Lemaître Center for Earth and Climate Research (TECLIM), Earth and Life Institute, Université  
catholique de Louvain, 1348 Louvain-la-Neuve, Belgium

*Correspondence to:* Zhengang Wang (wangzhg33@mail.sysu.edu.cn)

**Abstract.** There is increasing recognition that lateral soil organic carbon (SOC) fluxes due to erosion have  
10 imposed an important impact on the global C cycling. Field and experimental studies have been conducted to  
investigate this topic. It is useful to have a modelling tool that takes into account various soil properties and has  
flexible resolution and scale options, so that it can be widely used to study relevant processes and evaluate the  
effect of soil erosion on SOC cycling. This study presents a model that is capable of simulating SOC cycling on  
a dynamic landscape. It considers all the three C isotopes (<sup>12</sup>C, <sup>13</sup>C and <sup>14</sup>C) with flexible time step and vertical  
15 solution of the soil profile. The model gives a 3D representation of soil properties such as <sup>137</sup>Cs activity, SOC  
stock, and  $\delta^{13}\text{C}$  and  $\Delta^{14}\text{C}$  values. Using the same C cycling processes in stable, eroding and depositional areas,  
our model is able to reproduce the observed spatial and vertical patterns of C,  $\delta^{13}\text{C}$  values and  $\Delta^{14}\text{C}$  values. This  
indicates that physical soil redistribution is the main cause of the spatial variability of these C metrics.

### 1 Introduction

20 There is feedback between the biogeochemistry in the terrestrial system and the radiative forcing. Global warming  
will result in enhanced soil respiration (Bond-Lamberty et al., 2018) and decreased soil organic carbon (SOC)  
stock (Knorr et al., 2005). When more SOC is released to the atmosphere, the increased CO<sub>2</sub> will enhance the  
greenhouse effect (Davidson and Janssens, 2006). SOC is the largest organic C pool on the land with approximately  
1550 Pg C in the upper meter of soil (Lal, 2008). This is about two times of the C in the atmosphere (ca. 760 Pg  
25 C). The annual C flux between soil and the atmosphere is ca. 60 Pg C, which makes the atmosphere CO<sub>2</sub> is sensitive  
to SOC cycling. SOC stock is a balance between input fluxes and output fluxes, which is controlled by various  
factors such as soil structure, soil parent material, soil pH, climate and land use and management. Climate is an  
important controlling factor on SOC cycling as it is closely related to the rate of both C input and decomposition  
(e.g. Davidson and Janssens, 2006; Cox et al., 2000). The terrestrial net primary production and SOC  
30 decomposition rate generally decrease with increasing temperature (Koven et al., 2017). Globally, SOC stock  
decreases with increasing temperature (Jobbágy and Jackson, 2000). Land use is another important factor because  
different vegetation supplies SOC to the soil with different rates (Mahowald et al., 2017; Maia et al., 2010). The  
stable isotopic composition of SOC is affected by factors such as vegetation type (C<sub>3</sub> vegetation versus C<sub>4</sub>  
vegetation) and Suess effect (Tans et al., 1979). Also, SOC would become enriched in <sup>13</sup>C during the processes of  
35 SOC degradation due to preferential mineralization of <sup>12</sup>C (Natlhoffer and Fry, 1988).

Recent studies show that lateral soil redistribution by erosion could also impose an important impact on SOC



stock and soil-atmosphere C exchange (Doetterl et al., 2016;Chappell et al., 2016). During the erosion events, soil aggregates are broken by raindrop and overland flow, which can enhance the SOC decomposition (Van Hemelryck et al., 2011). In the eroding region, SOC in the topsoil is removed by erosion resulting in depletion of SOC. Soil minerals move upwards from below due to soil truncation are added SOC by inputs from plants (Harden et al., 1999). SOC deposited in the depositional settings is buried to depth and well preserved (Van Oost et al., 2012). This lateral redistribution of SOC and the consequent disturbance of SOC cycling of both eroding and depositional regions result in spatial variability in SOC stocks and properties. It was found that eroding sites are depleted of SOC compared to the stable sites while depositional sites are enriched in SOC compared to stable sites in agricultural fields (Li et al., 2007;Van Oost et al., 2005;Yoo et al., 2005). Soil redistribution could lead to difference of SOC stability between eroding and depositional areas. Berhe et al. (2008) found that SOC decomposes faster in the eroding areas compared to depositional areas through signatures of radioactive C isotope. Wang et al. (2014) reported that SOC mineralization rates in the eroding soil profiles are higher than that of depositional soil profiles from results of laboratory soil incubation. Radioactive C isotope gives information on the SOC turnover time, and it is a useful tool to investigate long-term SOC cycling (Trumbore, 2009). SOC redistribution was found to have an effect on SOC radioactive C isotope composition with eroding areas more negative compared to the depositional areas (Berhe et al., 2008).

Apart from the empirical studies mentioned above, various models have been developed to simulate soil erosion and SOC cycling. At the event scale, there are models simulating processes such as rainfall detachment, sediment entrainment and sediment transport (e.g. Hairsine and Rose, 1992b, a). Some models separate sediments into different sizes, and these models are suitable for simulations the size selectivity in erosion and deposition (Nearing, 1989;Van Oost et al., 2004). These models are further modified to simulate the selectivity of SOC in erosion and deposition (Wilken et al., 2017). Models based on USLE (Universal Soil Loss Equation) utilize annual mean precipitation as model input to simulate the long-term soil erosion (Renard et al., 1997). These models were further added processes of  $^{137}\text{Cs}$  deposition, decay and redistribution associated with soil particles, so that they can be calibrated using observed  $^{137}\text{Cs}$  data (Van Oost et al., 2003).

C turnover models have been developed under the condition of stable landscapes (i.e. free of erosion and deposition) to explore the effects of climate, land use and soil environment on SOC cycling. The decomposition of C is often represented by a first-order kinetic rate. Because the SOC is a complex of different components, it is often represented by various pools with respect to C input and decomposition rates in models such as Century (Parton et al., 1987), ICBM (Andren and Katterer, 1997) and RothC (Coleman and Jenkinson, 1995). C fractions obtained in laboratories have been related to C pools in models and used to calibrate model parameters to investigate the turnover of various C pools (Skjemstad et al., 2004;Zimmermann et al., 2007;Wang et al., 2015a). Other SOC properties were also used as constraints to calibrate and validate SOC models. For example,  $^{14}\text{C}$  signatures of SOC has been used to constrain parameters of a multiple-pool SOC model using Bayesian method (Ahrens et al., 2014).

These multiple-pool C models were further integrated with soil erosion models to make them applicable at eroding landscapes. The balance between the lateral SOC loss by erosion and in situ replacement of lost SOC by photosynthesis at eroding areas was investigated at the profile scale, and they found that proper management is important to maintain the dynamic replacement of lost C (Harden et al., 1999;Billings et al., 2010). At the depositional areas, a profile scale model integrating erosion and SOC cycling processes was calibrated using



observed SOC content and long-term depositional rate, and it was found that sedimentation rate plays an important role in determining burial efficiency of SOC in colluvial settings (Wang et al., 2015b). At the field scale, models that combine SOC redistribution by erosion and SOC dynamics are now well able to reproduce the spatial heterogeneity of SOC stock in fields under land uses with eroding areas depleted of SOC and depositional area enriched in SOC (Van Oost et al., 2005; Rosenbloom et al., 2001; Rosenbloom et al., 2006; Liu et al., 2003; Yoo et al., 2005). However, SOC models that both include C isotopes and are applicable in an eroding landscape are still lacking.

Here, we integrate SOC and soil erosion models and present a model tool that is capable of simulating SOC dynamics in a dynamic landscape. The objectives of this model tool are that (i) it should be a multiple C pool model that is able to represent the complexity of the SOC and to be related to the measurable SOC fractions; (ii) it should include various C isotopes so that it could not only represent these C metrics but also use them to constrain the model; (iii) it should be flexible in terms of spatial and temporal scales so that it would be applicable in various scenarios.

## 2 Methods

Here we present the WATEM\_C model that simulates the redistribution of eroded soil and associated C within the catchment and its effects on the dynamics of SOC. The soil redistribution by water erosion is based on the WATEM model (Van Oost et al., 2000) while simulation of C dynamics is based on a three-pool C model (Wang et al., 2015a). All the three C isotopes ( $^{12}\text{C}$ ,  $^{13}\text{C}$  and  $^{14}\text{C}$ ) are included in our model. Soil advection and diffusion through the soil profile are also included in the model. The model uses flexible time step and vertical resolution of the soil profile so that it can be applied in various settings.

### 2.1 C erosion by water

RUSLE (Revised Universal Soil Loss Equation) (Renard et al., 1997) is used to simulate the long-term potential water erosion ( $E_{\text{pot}}$ ;  $\text{kg m}^{-2} \text{yr}^{-1}$ ):

$$E_{\text{pot}} = R * K * L * S * C * P \quad (1)$$

where  $R$  is the rainfall erosivity ( $\text{MJ mm ha}^{-1} \text{h}^{-1} \text{yr}^{-1}$ ),  $K$  is soil erodibility ( $\text{kg h MJ}^{-1} \text{mm}^{-1}$ ),  $L$  and  $S$  are slope steep and length factors, and  $C$  and  $P$  are factors for the cover management and support practices.

The local erosion rate is considered to equal to the potential erosion rate if the potential erosion rate does not exceed the local transport capacity. The local transport capacity ( $T_c$ ;  $\text{kg m}^{-1} \text{yr}^{-1}$ ) is calculated as:

$$T_c = k_{tc} * E_{\text{pot}} \quad (2)$$

where  $k_{tc}$  is the transport capacity coefficient (m). In a grid cell, if its sediment inflow exceeds its local transport capacity, the amount of material transported through the grid equals to the local transport capacity while the remainder is deposited in the grid.

The mobilization of SOC by erosion ( $C_{\text{ero}}$ ,  $\text{kg m}^{-2} \text{yr}^{-1}$ ) is estimated as:

$$C_{\text{ero}} = C_{\text{top}} * R_{\text{ero}} * ER_{\text{ero}} \quad (3)$$

where  $C_{\text{top}}$  is the C content of the top soil layer (%),  $R_{\text{ero}}$  is the local erosion rate ( $\text{kg m}^{-2} \text{yr}^{-1}$ ),  $ER_{\text{ero}}$  is C enrichment ratio in the eroded sediments that equals to the ratio of C content in the eroded sediments to that in the source soils.



The deposited C ( $C_{\text{depo}}$ ,  $\text{kg m}^{-2} \text{yr}^{-1}$ ) can be calculated as:

$$C_{\text{depo}} = C_{\text{sed}} * R_{\text{depo}} * ER_{\text{depo}} \quad (4)$$

115 where  $C_{\text{sed}}$  is the C content in the transported sediments (%),  $R_{\text{depo}}$  is the local deposition rate ( $\text{kg m}^{-2} \text{yr}^{-1}$ ),  $ER_{\text{depo}}$  is C enrichment ratio in the deposited sediments that equals to the ratio of the C content in the deposited sediments to that in the bulk transported sediments reaching the depositional sites.

The C enrichment ratios in the mobilized sediments at the erosion sites or in the deposited sediments at the deposited sites are found to be closely related to the local erosion or deposition rates (Wang et al., 120 2010; Schiettecatte et al., 2008). Thus, the C enrichment ratios of the mobilized and deposited sediments are calculated as:

$$ER_{\text{ero}} = a * e^{b * R_{\text{ero}}} + 1 \quad (5)$$

$$ER_{\text{depo}} = -0.5e^{d * R_{\text{depo}}} + 1 \quad (6)$$

where a, b, and d are coefficients.

## 125 2.2 Soil C turnover

In our model, the three C isotopes ( $^{12}\text{C}$ ,  $^{13}\text{C}$  and  $^{14}\text{C}$ ) are distinguished. As called in the Century model (Parton et al., 1987), each C isotope is divided into three pools that are referred to as active, slow, and passive pools. The decomposition of these C pools is described using the following differential equations:

$$\frac{d {}^n A(z,t)}{dt} = {}^n i(z) - {}^n k_1 r(z) {}^n A(z,t) \quad (7)$$

$$130 \frac{d {}^n S(z,t)}{dt} = h_{AS} {}^n k_1 r(z) {}^n A(z,t) - {}^n k_2 r(z) {}^n S(z,t) \quad (8)$$

$$\frac{d {}^n P(z,t)}{dt} = h_{AP} {}^n k_1 r(z) {}^n A(z,t) + h_{SP} {}^n k_2 r(z) {}^n S(z,t) - {}^n k_3 r(z) {}^n P(z,t) \quad (9)$$

135 where  ${}^n A(z,t)$ ,  ${}^n S(z,t)$ , and  ${}^n P(z,t)$  (Mg C ha<sup>-1</sup>) are the active, slow, and passive pools of C isotope n at depth z (m) and time t (year), respectively;  ${}^n i(z)$  (Mg C ha<sup>-1</sup> yr<sup>-1</sup>) is the input of C isotope n at depth z (m);  $h_{AS}$  is the humification coefficients from the active pool to the slow pool,  $h_{AP}$  from the active pool to the passive pool, and  $h_{SP}$  from the slow pool to the passive pool, respectively;  $r(z)$  is a coefficient modifying the variation of C mineralization rate, which denotes the effect of local environmental factors (temperature, humidity, aeration, etc.) at depth z (m); and  ${}^n k_1$ ,  ${}^n k_2$ , and  ${}^n k_3$  (yr<sup>-1</sup>) are the turnover rates at the reference condition (i.e.  $r(z) = 1$ ) of the active, slow, and passive pools of C isotope n, respectively.

$^{12}\text{C}$  is preferentially lost through microbial respiration compared to  $^{13}\text{C}$  and  $^{14}\text{C}$  due to its lower atomic weight 140 (Natelhoffer and Fry, 1988). We used discrimination ratio to denote the difference in mineralization between isotopes, and thus the decomposition rate of a  $^{13}\text{C}$  pool ( $^{13}K_m$ , yr<sup>-1</sup>) can be calculated as:

$$^{13}K_m = R_{\text{disc}_{13}} * ^{12}K_m \quad (10)$$

where  $R_{\text{disc}_{13}}$  is the discrimination ratio between  $^{13}\text{C}$  and  $^{12}\text{C}$ ,  $^{12}K_m$  is the decomposition rate of the corresponding  $^{12}\text{C}$  pool.



145 Similarly, the decomposition rate of a  $^{14}\text{C}$  pool ( $^{14}\text{K}_m$ ,  $\text{yr}^{-1}$ ) can be calculated as:

$$^{14}\text{K}_m = R_{\text{disc},14} * ^{12}\text{K}_m \quad (11)$$

where  $R_{\text{disc},14}$  is the discrimination ratio between  $^{14}\text{C}$  and  $^{12}\text{C}$ .

$r$  parameter represents the effect of environmental factors affecting C respiration at a given depth, and it is calculated as:

150  $r(z) = r_0 e^{-r_e z} \quad (12)$

where  $r_0$  is the value of  $r$  parameter at the top soil layer, and  $r_e$  ( $\text{m}^{-1}$ ) is an exponential decreasing coefficient .

The input of the C isotopes from plant roots decreases exponentially with depth (Gerwitz and Page, 1974; Van Oost et al., 2005):

$$^n i(z) = ^n i_0 e^{-i_e z} \quad (13)$$

155 where  $^n i_0$  is the input of C isotope  $n$  at the top soil layer ( $\text{Mg C ha}^{-1} \text{ yr}^{-1}$ );  $^n i(z)$  ( $\text{Mg C ha}^{-1} \text{ yr}^{-1}$ ) is the input of C isotope  $n$  at depth  $z$  (m); and  $i_e$  ( $\text{m}^{-1}$ ) is an exponential decreasing coefficient.

The  $\delta^{13}\text{C}$  values are expressed in terms of permil (‰) deviation:

$$\delta^{13}\text{C} = \left( \frac{(^{13}\text{C}/^{12}\text{C})_{\text{Sample}}}{(^{13}\text{C}/^{12}\text{C})_{\text{PDB}}} - 1 \right) * 1000 \quad (14)$$

160 where  $(^{13}\text{C}/^{12}\text{C})_{\text{Sample}}$  is the abundance ratio of  $^{13}\text{C}$  to  $^{12}\text{C}$  of the soil sample, and  $(^{13}\text{C}/^{12}\text{C})_{\text{PDB}}$  is the ratio of the Pee Dee Belemnite (PDB) as the original standard.

Thus, the  $^{13}\text{C}$  input can be calculated as:

$$^{13}i = (^{13}\text{C}/^{12}\text{C})_{\text{PDB}} * \left( 1 + \frac{\delta^{13}\text{C}(t)}{1000} \right) * ^{12}i \quad (15)$$

where  $^{13}i$  is the  $^{13}\text{C}$  input ( $\text{Mg C ha}^{-1} \text{ yr}^{-1}$ ) from plant,  $^{12}i$  is the  $^{12}\text{C}$  input from plant,  $\delta^{13}\text{C}(t)$  is  $\delta^{13}\text{C}$  values of C input at time  $t$  (yr).

165 We use the atmospheric  $\Delta^{14}\text{C}$  record as a proxy for the isotopic ratio of C input via root and leaf litter input (Hua and Barbetti, 2004). In this paper, the following definition of  $\Delta^{14}\text{C}$  (‰) is used (Stuiver and Polach, 1977):

$$\Delta^{14}\text{C} = \left( \frac{(^{14}\text{C}/^{12}\text{C})_{\text{Sample}}}{A_{\text{ABS}}} - 1 \right) * 1000 \quad (16)$$

where  $(^{14}\text{C}/^{12}\text{C})_{\text{Sample}}$  denotes the  $^{14}\text{C}:^{12}\text{C}$  ratio of the sample, and  $A_{\text{ABS}}$  denotes the  $^{14}\text{C}:^{12}\text{C}$  ratio of the standard.  $A_{\text{ABS}}$  is set to be  $1.176 * 10^{-12}$  (Karlen et al., 1965; Stuiver, 1980).

170 The  $^{14}\text{C}$  input can then be calculated as:

$$^{14}i = A_{\text{ABS}} * \left( 1 + \frac{\Delta^{14}\text{CO}_2^{\text{ATM}}(t)}{1000} \right) * ^{12}i \quad (17)$$

where  $^{14}i$  is  $^{14}\text{C}$  input ( $\text{Mg C ha}^{-1} \text{ yr}^{-1}$ ) from plant, and the  $\Delta^{14}\text{CO}_2^{\text{ATM}}(t)$  is the atmospheric  $\Delta^{14}\text{C}$  signals at time  $t$  (yr).



### 2.3 Soil profile evolution due to erosion

175 In the model, soil profiles are represented as a series of soil layers with equal depths. Given that C input and SOC  
decomposition rate are related with soil depth, SOC cycling is simulated in each layer independently. Because  
erosion and deposition change the depth of soil profiles, the model updates the depth of soil profiles and the carbon  
content of each soil layer every time step. At the eroding locations, soils are removed from the top layer and the  
soil profile is truncated by the amount of eroded soil. At the meantime, SOC is also lost with the local C enrichment  
180 ratio. To keep the soil layer with fixed thickness, soils and associated SOC from soil layers below are incorporated  
into the upper soil layer at the erosion rate. At the depositional locations, because the top layer is buried by the  
deposited sediments at the deposition rate, soils and associated SOC are moved downward. For all the soil profiles,  
the component pools of each C isotopes of every layer are updated by homogeneously mixing the component  
materials every time step.

### 185 2.4 Advection and diffusion

The vertical transport of mineral and organic components of soil is a complex phenomenon driven by a number of  
distinct mechanisms such as bioturbation (Johnson et al., 2014; Jagercikova et al., 2017), and chemical mobilization  
(Taylor et al., 2012). We use the advection-diffusion equation to model vertical transport:

$$\frac{dF(z,t)}{dt} = K(z) \frac{d^2}{dz^2} F(z,t) - v(z) \frac{dF(z,t)}{dz} \quad (18)$$

190 where  $F(z,t)$  is the concentration of a soil constitute (such as a C isotope pool or  $^{137}\text{Cs}$ ) at depth  $z$  (m) at time  $t$  (yr),  
 $v(z)$  ( $\text{m yr}^{-1}$ ) is the advection term at depth  $z$  (m) and  $K(z)$  ( $\text{m yr}^{-1}$ ) is a diffusion-type mixing coefficient at depth  
 $z$  (m).

$K$  and  $v$  are both depth-dependent and are represented using a sigmoidal scaling function:

$$v(z) = \frac{v_0}{1 + e^{(v_d(z-ct))}} \quad (19)$$

195 where  $v_d$  ( $\text{m}^{-1}$ ) is the depth-attenuation of advection,  $ct$  (m) is a constant that is set to 0.15 m, and  $v_0$  ( $\text{m yr}^{-1}$ ) is  
the value of  $v$  at the top soil layer.

$$K(z) = \frac{K_0}{1 + e^{(K_d(z-ct))}} \quad (20)$$

where  $K_d$  ( $\text{m}^{-1}$ ) is the depth-attenuation of diffusion, and  $K_0$  ( $\text{m yr}^{-1}$ ) is the value of  $K$  at the top soil layer.

### 2.5 $^{137}\text{Cs}$ dynamics

200  $^{137}\text{Cs}$  originates from bomb experiments between 1950 and 1970. It falls to the Earth's surface primarily in  
association with precipitation and is rapidly adsorbed to soil by clay materials. As the fallout is well constrained,  
 $^{137}\text{Cs}$  has been widely used for tracing the movement of soil and sediment particles in erosion studies (Ritchie and  
McHenry, 1990). The model reads the values of the local  $^{137}\text{Cs}$  fallout. The model then simulates the redistribution  
of  $^{137}\text{Cs}$  by soil erosion and deposition at the land surface associated with soil particles. The model also simulates  
205 the downward movement of  $^{137}\text{Cs}$  in the soil profile by advection and diffusion. The decay of  $^{137}\text{Cs}$  (half-life of  
30.23 year) is also represented in the model.



## 2.6 Model implementation

In order to make the model applicable at various temporal and spatial resolutions, the time step of model iteration and vertical resolution of the soil profile were not fixed, but modifiable as parts of the model input parameters. Given the long-term temporal iteration in SOC cycling processes and the possible large spatial regions where the model may apply, the model was developed using a computation-efficient language (Pascal). The compiled executable file can then be called in other environment such as R (R Development Core Team, 2011) where the preparation of the input maps is easier. In our model, the default values of the input parameters were given, and at the same time the user are allowed to assign custom values to the input parameters in the R environment when calling the executable file. The description and relevant parameters regarding SOC cycling are listed in Table 1.

## 2.7 Model application

A set of three scenarios was assumed in order to investigate the effect of advection and diffusion and lateral soil redistribution by erosion on the spatial and vertical distribution of SOC, and  $\delta^{13}\text{C}$  and  $\Delta^{14}\text{C}$  values at the landscape scale. Scenario 1: scenario without advection or diffusion or lateral soil redistribution; Scenario 2: scenario with vertical advection and diffusion but without lateral soil redistribution and Scenario 3: scenario with both advection, diffusion and lateral soil redistribution. In order to investigate the effect of plant type change and Suess effect on the  $\delta^{13}\text{C}$  values of soil profiles, the model was applied in another set of three scenarios. Given that advection and diffusion is common in soils, we used the scenario with only advection and diffusion as the reference scenario, i.e. Scenario 2 defined above. The other two scenarios are Scenario 4 with plant type change and Scenario 5 with Suess effect.

## 3 Results

### 3.1 $^{137}\text{Cs}$

Our simulation shows that, without advection and diffusion, the deposited  $^{137}\text{Cs}$  is restrained on the surface of soils (Figure 1a). Advection and diffusion transfers soil materials and associated  $^{137}\text{Cs}$  to the depth, and the amount of transfer is related to the rate of advection and diffusion (Figure 1b). On the eroding landscape, our simulation shows that eroding soil profile is depleted of  $^{137}\text{Cs}$  compared to the stable soil profile, while the depositional profile is enriched in  $^{137}\text{Cs}$  in comparison to the stable soil profile (Figure 1c). Also,  $^{137}\text{Cs}$  in the depositional profile reaches deeper depth compared to the stable soil profile.

### 3.2 SOC

Our model is able to reproduce the general pattern of SOC profile of decreasing SOC content with depth in all scenarios despite of rates of advection, diffusion, erosion or deposition (Figure 2). In Scenario 2, higher rates of soil advection and diffusion result in more SOC transferred to the depth, and therefore the difference of SOC content between top layers and bottom layers is smaller under the condition of higher soil advection and diffusion rate compared to SOC profiles of lower advection and diffusion rate (Figure 2b). In Scenario 3, eroding soil profiles contain less SOC compared to the stable soil profiles free of erosion/deposition, while soil profiles at the depositional area are enriched in SOC compare to the stable soil profile (Figure 2c).



### 3.3 $\delta^{13}\text{C}$ values

In Scenario 1, the  $\delta^{13}\text{C}$  profile shows no variation with depth (Figure 3a). In Scenario 2, the  $\delta^{13}\text{C}$  profile decreases with depth (Figure 3b). The  $\delta^{13}\text{C}$  values of soil profile with higher soil advection and diffusion rates are more negative than that with lower soil advection and diffusion rates (Figure 3b). In Scenario 3, the  $\delta^{13}\text{C}$  values of the eroding profile is less negative than that of the stable soil profile, while soil profiles at the depositional area have more negative  $\delta^{13}\text{C}$  values compared to the stable soil profile (Figure 3c). Our simulation shows that  $\delta^{13}\text{C}$  values increase significantly when the vegetation is converted from  $\text{C}_3$  vegetation to  $\text{C}_4$  vegetation (Figure 4). When Suess effect is considered, the  $\delta^{13}\text{C}$  values are lower than that in scenarios that do not consider Suess effect (Figure 4).

### 3.4 $\Delta^{14}\text{C}$ values

Our model is able to reproduce the general pattern of decreasing  $\Delta^{14}\text{C}$  values with depth in all scenarios despite of rates of soil advection, diffusion, erosion or deposition (Figure 5). In Scenario 2, Soil profiles with higher rates of advection and diffusion have higher  $\Delta^{14}\text{C}$  values compared to profiles with lower vertical transfer rates (Figure 5b). In scenario 3, eroding soil profiles has lower  $\Delta^{14}\text{C}$  values compared to the stable soil profiles, while soil profiles at the depositional area are enriched in  $^{14}\text{C}$  compared to the stable soil profile (Figure 5c).

### 3.5 Spatial variability of soil properties

The model is able to generate a reasonable pattern of soil redistribution with erosion occurring in upland areas and deposition occurring in footslope areas or valleys (Figure 6b). Soil redistribution results in higher  $^{137}\text{Cs}$  inventories in depositional area than eroding area (Figure 6c). The model is also able to generate spatial variability of SOC stock and properties induced by erosion. The depositional area is enriched in SOC compared with eroding area (Figures 6d and 6e). SOC in the depositional area has lower  $\delta^{13}\text{C}$  values (Figures 6f and 6g) and higher  $\Delta^{14}\text{C}$  values (Figures 6h and 6j) compared to that in the eroding area.

## 4 Discussion

In Scenario 1, the shape of the SOC profile is determined by the vertical patterns of SOC input and decomposition rates, both of which decrease with depth. The fact that the basic shape of the SOC profile can be well represented in Scenario 1 shows that the pattern of C input and decomposition rates is the primary controlling factor on the SOC profile while other factors such as advection and diffusion, erosion or deposition are relatively secondary (Figure 2a). It is natural that higher rates of advection and diffusion would result in more SOC to be transferred to deep layers (Figure 2b). Given that it is less favorable for SOC to be mineralized in deep layers, the transferred SOC by advection and diffusion to the depth would be better preserved. Simulations in Scenario 2 show that SOC stock in the top 1 m under the condition of high advection and diffusion rate ( $K=0.09$ ,  $v=0.018$ ) is ca. 14% higher than that under the condition of low advection and diffusion rate ( $K=0.05$ ,  $v=0.01$ ). Our model can not only reproduce the vertical pattern of SOC distribution in the soil profile, but that it can also reproduce the spatial variability of SOC stock due to soil redistribution. The simulations under Scenario 3 are consistent with observations that soil erosion results in spatial variability of SOC stock (VandenBygaert et al., 2012; Van Oost et al., 2005; Yoo et al., 2005). This spatial variability was attributed to the replacement of lost at the eroding area and partially preservation of buried SOC in the depositional area (Wang et al., 2015b; Harden et al., 1999; Van Oost et al., 2005).



In Scenario 1, each soil layer is independent from other soil layers, i.e. there is no mass fluxes between soil layers due to the negelation of advection, diffusion and soil redistribution. In this case, each soil layer has its C input and decomposition rates. The  $\delta^{13}\text{C}$  value of each soil layer is therefore determined by the discrimination ratio between  $^{13}\text{C}$  and  $^{12}\text{C}$ . If this discrimination ratio is the same between soil layers as implemented in this model, the equilibrium  $\delta^{13}\text{C}$  profile would be vertically constant (Figure 3a). Due to the fact that the condition of no soil advection and diffusion is not realistic, vertically constant  $\delta^{13}\text{C}$  profile with depth is rarely reported. When vertical advection and diffusion are considered as in Scenario 2, the transferred SOC from upper layers are isotopically heavier due to degradation compared to the fresh input from plant. This results in an increase of  $\delta^{13}\text{C}$  values with soil depth (Figure 3b). Our simulation shows that vertical soil advection and diffusion can be one of the main causes of the widely observed increase of  $\delta^{13}\text{C}$  profiles with depth (Figure 7). At the same depth, soil profile of low soil advection and diffusion rate contains more degraded SOC than profile of high soil advection and diffusion rate, and therefore soil profile of low soil advection and diffusion rate has less negative  $\delta^{13}\text{C}$  values. Because erosion and deposition will truncate or bury the original  $\delta^{13}\text{C}$  profiles, this results in the fact that the eroding soil profile will have higher  $\delta^{13}\text{C}$  values compared to the stable soil profile while the soil profiles at the depositional sites will have lower  $\delta^{13}\text{C}$  values in comparison to the stable soil profile (Figure 3c). This is consistent with the observation made in the cropland in Begium (Figure 7). Also, this discrepancy will be more distinct when the erosion or deposition rates become higher. Our simulation shows that soil redistribution by erosion can also cause spatial variability of  $\delta^{13}\text{C}$  values on an eroding land.

Our model is able to reproduce the widely observed decrease of  $\Delta^{14}\text{C}$  values with depth in soil profiles (Figure 5). Also, the model can capture the signal of bomb carbon with  $\Delta^{14}\text{C}$  values at the surface layer being positive. In Scenario 1 with no mass fluxes between soil layers,  $\Delta^{14}\text{C}$  values is mainly a metrics for the turnover rate or residence time of SOC in each layer. The simulated vertical decrease of  $\Delta^{14}\text{C}$  values is attributed to the vertical variation of environmental conditions that become less favorable for C mineralization. As discussed for  $\delta^{13}\text{C}$  profiles, at the same depth soil profile of low soil advection and diffusion rate contains more degraded and old SOC than profile of high soil advection and diffusion rate, and therefore soil profile of low soil advection and diffusion rate has more negative  $\Delta^{14}\text{C}$  values (Figure 5b). Similar to  $\delta^{13}\text{C}$  profiles, erosion and deposition also have a truncation or burial effect of on the  $\Delta^{14}\text{C}$  profile and this results in the simulation that the eroding soil profiles have more negative  $\Delta^{14}\text{C}$  values compared to the stable soil profile while the profiles at the depositional sites have less negative  $\Delta^{14}\text{C}$  values than the stable soil profile (Figure 5c). Our simulation is consistent with the observation from an eroding hillslope in northern California by Berhe et al. (2008) (Figure 8). The causes of more negative  $\Delta^{14}\text{C}$  values in eroding soil profiles are mainly attributed to the exposure of old SOC from depth, while the observed less negative  $\Delta^{14}\text{C}$  values in depositional profiles is due to the burial of young SOC from eroding areas.

WATEM\_C model focuses on the catchment scale, which allows it to account for processes of both erosion and deposition. It is a spatially distributed model with parcel maps denoting various land use types. Also, it allows accounting for soil conservation measurements, which enables the model to investigate anthropogenic effects (such as land use and management) on erosion and SOC cycling. Compared to previous models, the model presented here is more comprehensive. It includes SOC cycling process and the redistribution of soil and associated SOC by erosion. It is a three-pool C model that discriminates C isotopes ( $^{12}\text{C}$ ,  $^{13}\text{C}$  and  $^{14}\text{C}$ ). Thus, it could not only give a three-dimension representation of C, but also C properties such as  $\delta^{13}\text{C}$  and  $\Delta^{14}\text{C}$  values (Figure 6). The fact that



our model could reproduce the observed spatial variability of  $^{137}\text{Cs}$  activity, SOC stock,  $\delta^{13}\text{C}$  values and  $\Delta^{14}\text{C}$  values indicates that our model captures the main processes regarding soil redistribution and SOC cycling. The default values of most of the parameters was set in the executable file generated in Pascal, but they can be assigned to custom values before running the executable file in R. This allows the model to be applied in various scenarios by setting relevant parameter values. The model is programmed in a computational efficiency language (Pascal), which makes it suitable to include more C pools and isotopes. Also, the vertical resolution of the soil profile and the temporal resolution of the model iteration is set to be flexible in our model. The users could modify these parameter based on the requirements of circumstances. The arrangement that the model can be called in R makes it easier to prepare various input maps and to proceed the output of the model. However, it requires the users to have experiences in coding in R. The model is designed to simulate only one period with temporally varying inputs on  $^{137}\text{Cs}$  fallout,  $^{13}\text{C}$  and  $^{14}\text{C}$  input. For the cases of temporal variations such as C input or erosion caused by land use change, the current version of the model is not able to represent these processes.

## 5 Conclusions

This paper presents a model (WATEM\_C) that is capable of simulating SOC dynamics on an eroding landscape. It allows tracking the redistribution of soils and associated  $^{137}\text{Cs}$  and SOC within the catchment. The model captures the soil profile evolution due to erosion and deposition. The SOC dynamics was simulated using a 3 pool C cycling model. All the three C isotopes ( $^{12}\text{C}$ ,  $^{13}\text{C}$  and  $^{14}\text{C}$ ) are considered in the model and are discriminated with different cycling rates. The model uses flexible time step and vertical solution of the soil profile. It gives a 3D representation of soil properties such as  $^{137}\text{Cs}$  activity, SOC stock,  $\delta^{13}\text{C}$  values and  $\Delta^{14}\text{C}$  values. The model is able to reproduce the observed spatial pattern of the SOC stock that eroding soil profiles are depleted of SOC compared to the stable soil profile while depositional soil profile is enriched of SOC than the stable soil profile. Our simulation is consistent with the observation that the  $\delta^{13}\text{C}$  values of the eroding profile is less negative than that of the stable soil profile, while soil profiles at the depositional area have more negative  $\delta^{13}\text{C}$  values compared to the stable soil profile. Our model reproduces the observation that eroding soil profiles has lower  $\Delta^{14}\text{C}$  values compared to the stable soil profiles, while soil profiles at the depositional area are enriched in  $^{14}\text{C}$  compared to the stable soil profile. The fact that the spatial patterns of these SOC metrics can be reproduced using the same C cycling processes indicates that physical soil redistribution is the main causes of these spatial variabilities and that our model captures the most important processes and mechanisms in the SOC cycling on an eroding landscape. We envisage WATEM\_C to be a useful tool in simulating the SOC cycling on an eroding landscape with the wide cover of various soil properties and flexible choices of resolution options and scenario settings.

*Code availability.* Codes for the model is available at [https://github.com/wangzhg33/WATEM\\_C-version1.0](https://github.com/wangzhg33/WATEM_C-version1.0) (last access: 20 September 2019).

*Author contributions.* All the authors were involved in the design of the model. ZW further developed WATEM\_C based on the WATEM model developed by KVO. ZW and KVO wrote the paper together.



355 *Competing interests.* The authors declare that they have no conflict of interest.

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360 Tables

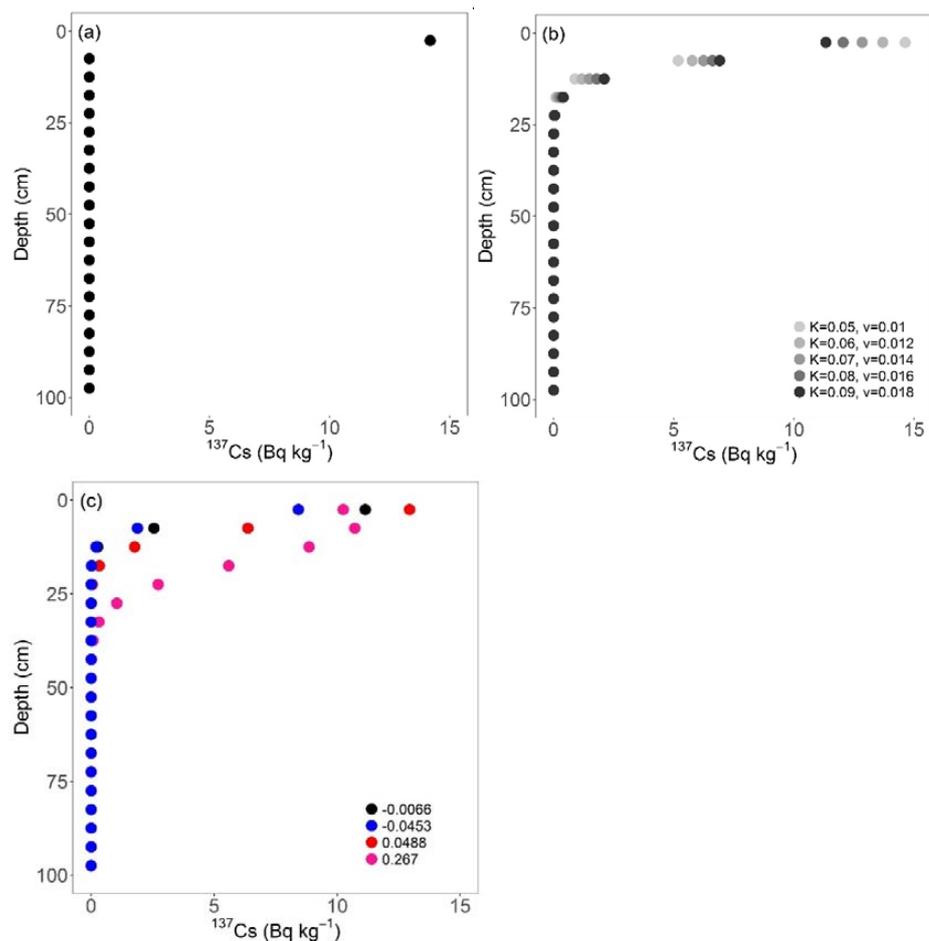
**Table 1. Values of parameters on SOC cycling used this study**

Parameter	Description	Unit	Values
$^{12}k_1$	turnover rates of the active $^{12}C$ pool	yr <sup>-1</sup>	2.1
$^{12}k_2$	turnover rates of the active $^{13}C$ pool	yr <sup>-1</sup>	0.03
$^{12}k_3$	turnover rates of the active $^{14}C$ pool	yr <sup>-1</sup>	0.002
$h_{AS}$	humification coefficients from the active pool to the slow pool	-	0.12
$h_{AP}$	humification coefficients from the active pool to the passive pool	-	0.01
$h_{SP}$	humification coefficients from the slow pool to the passive pool	-	0.01
$r_0$	the $r$ parameter at the top soil layer	-	1
$i_{root}$	C input from root	Mg C ha <sup>-1</sup> yr <sup>-1</sup>	2.0
$i_{resi}$	C input from leaf litter	Mg C ha <sup>-1</sup> yr <sup>-1</sup>	0.5
$r_e$	exponential decreasing coefficient of $r$ with depth	m <sup>-1</sup>	3.30
$i_e$	exponential decreasing coefficient for the root C input with depth	m <sup>-1</sup>	20
$R_{disc\_13}$	discrimination ratio between $^{13}C$ and $^{12}C$	-	0.9977
$R_{disc\_14}$	discrimination ratio between $^{14}C$ and $^{12}C$	-	0.996

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Figures



370 Figure 1: The simulated  $^{137}\text{Cs}$  activity ( $\text{Bq kg}^{-1}$ ) profile in (a) Scenario 1, (b) Scenario 2, and (c) Scenario 3. See Section 2.7 for the descriptions of scenarios. In b,  $K$  ( $\text{m}^2 \text{yr}^{-1}$ ) is the diffusion coefficient and  $v$  ( $\text{m yr}^{-1}$ ) is the advection term (Eq. 18). In c, the numbers in the legend are the erosion or deposition rates ( $\text{cm yr}^{-1}$ ) with negative values indicating erosion and positive values indicating deposition.

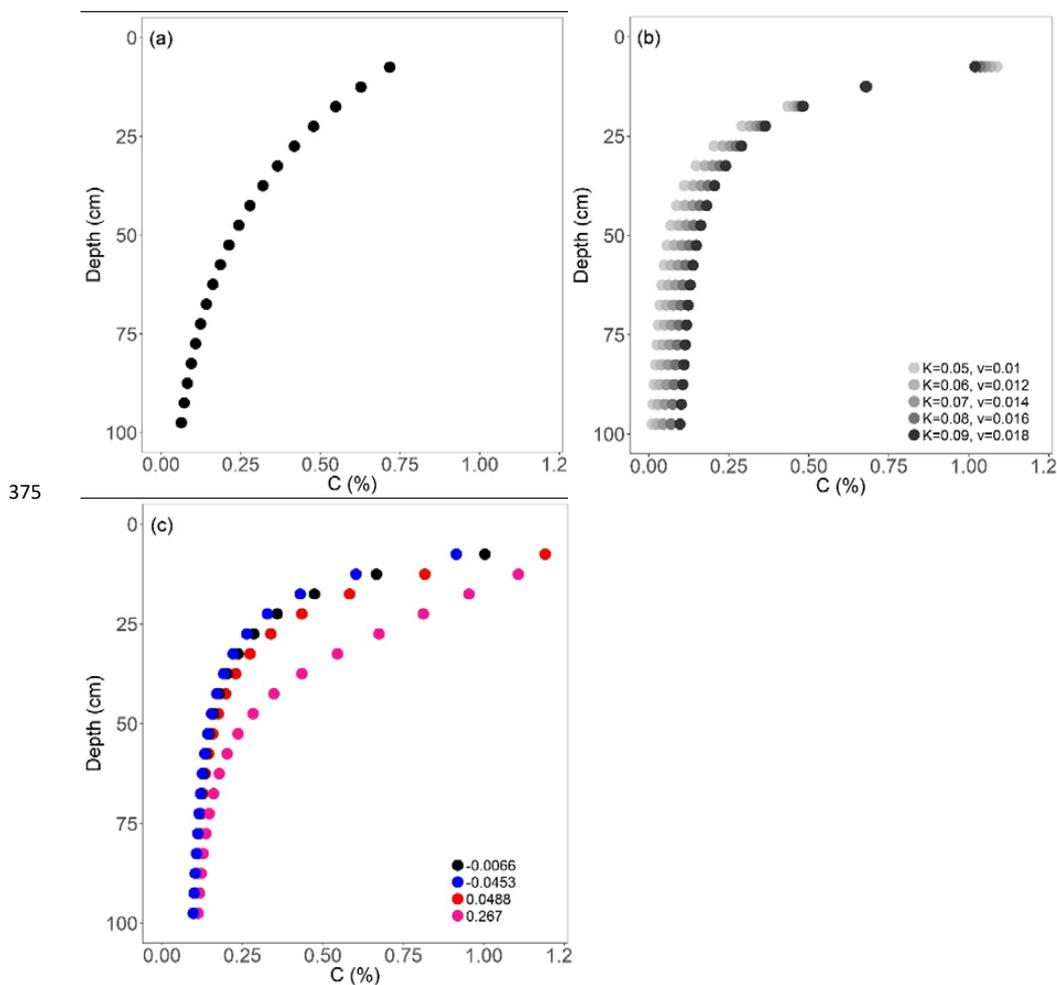


Figure 2: The simulated C content profiles in (a) Scenario 1, (b) Scenario 2, and (c) Scenario 3. See Section 2.7 for the descriptions of scenarios. In b,  $K$  ( $\text{m}^2 \text{yr}^{-1}$ ) is the diffusion coefficient and  $v$  ( $\text{m yr}^{-1}$ ) is the advection term (Eq. 18). In c, the numbers in the legend are the erosion or deposition rates ( $\text{cm yr}^{-1}$ ) with negative values indicating erosion and positive values indicating deposition.

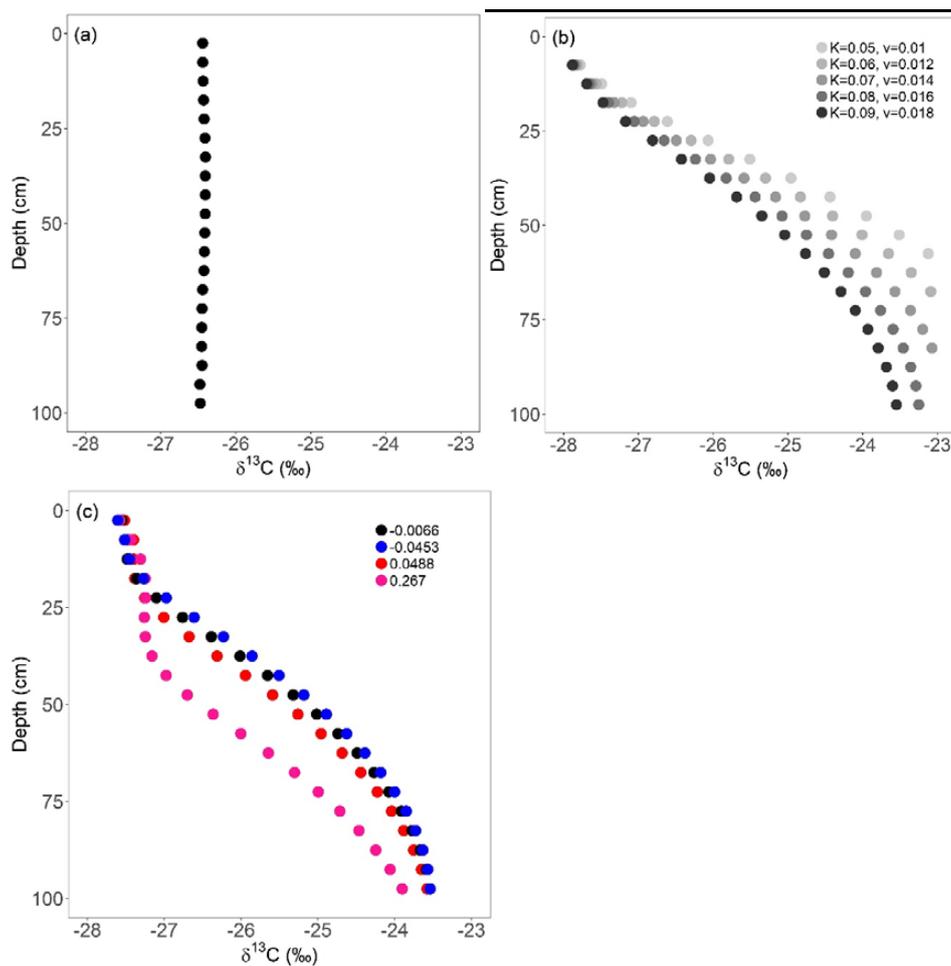


Figure 3: The simulated  $\delta^{13}\text{C}$  profiles in (a) Scenario 1, (b) Scenario 2, and (c) Scenario 3. See Section 2.7 for the  
385 descriptions of scenarios. In b,  $K$  ( $\text{m}^2 \text{yr}^{-1}$ ) is the diffusion coefficient and  $v$  ( $\text{m yr}^{-1}$ ) is the advection term (Eq. 18). In  
c, the numbers in the legend are the erosion or deposition rates ( $\text{cm yr}^{-1}$ ) with negative values indicating erosion and  
positive values indicating deposition.

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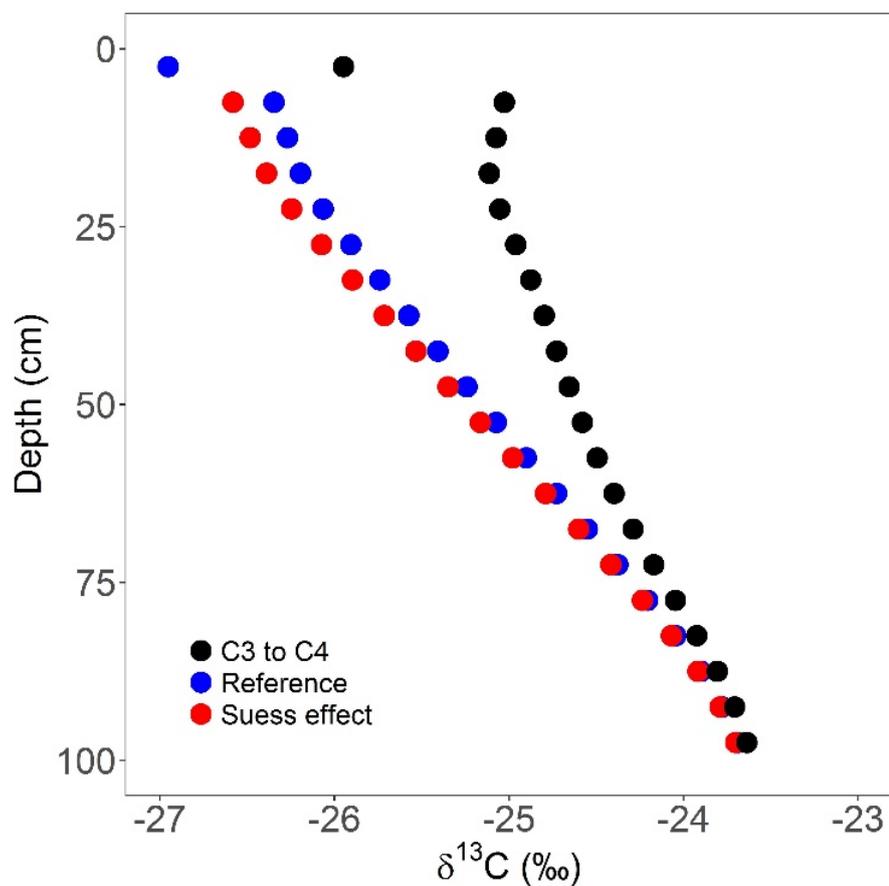
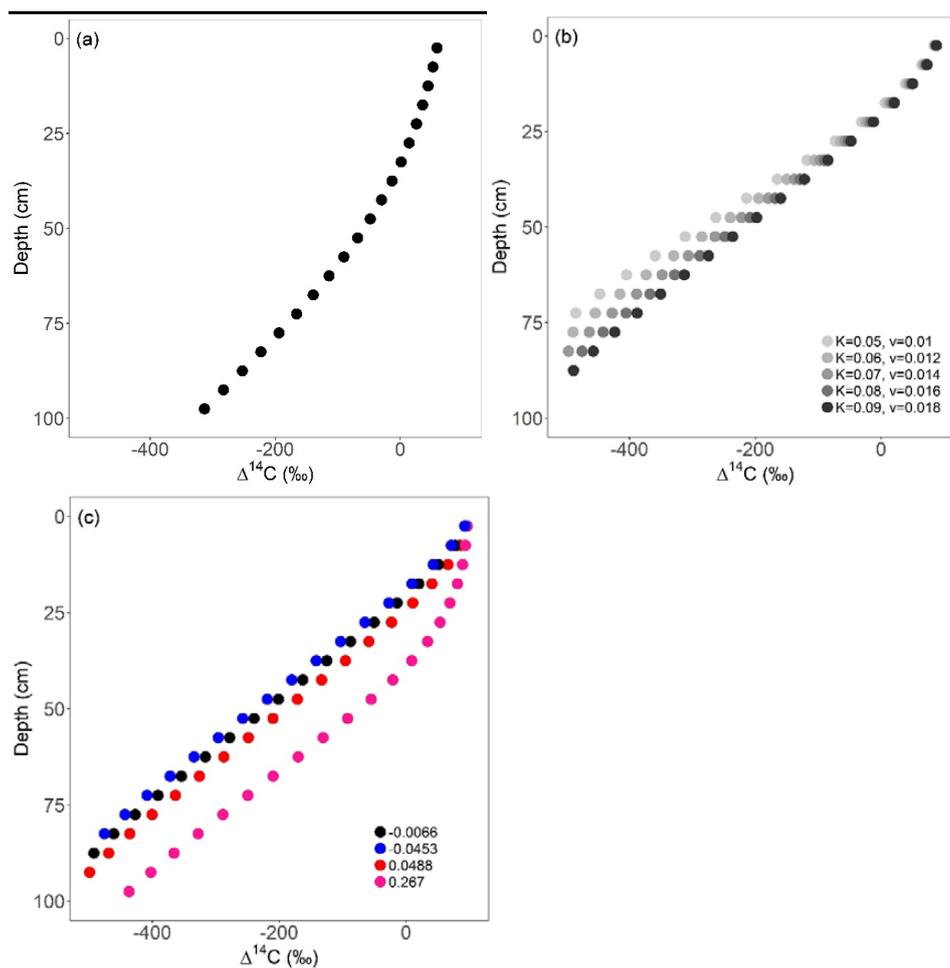


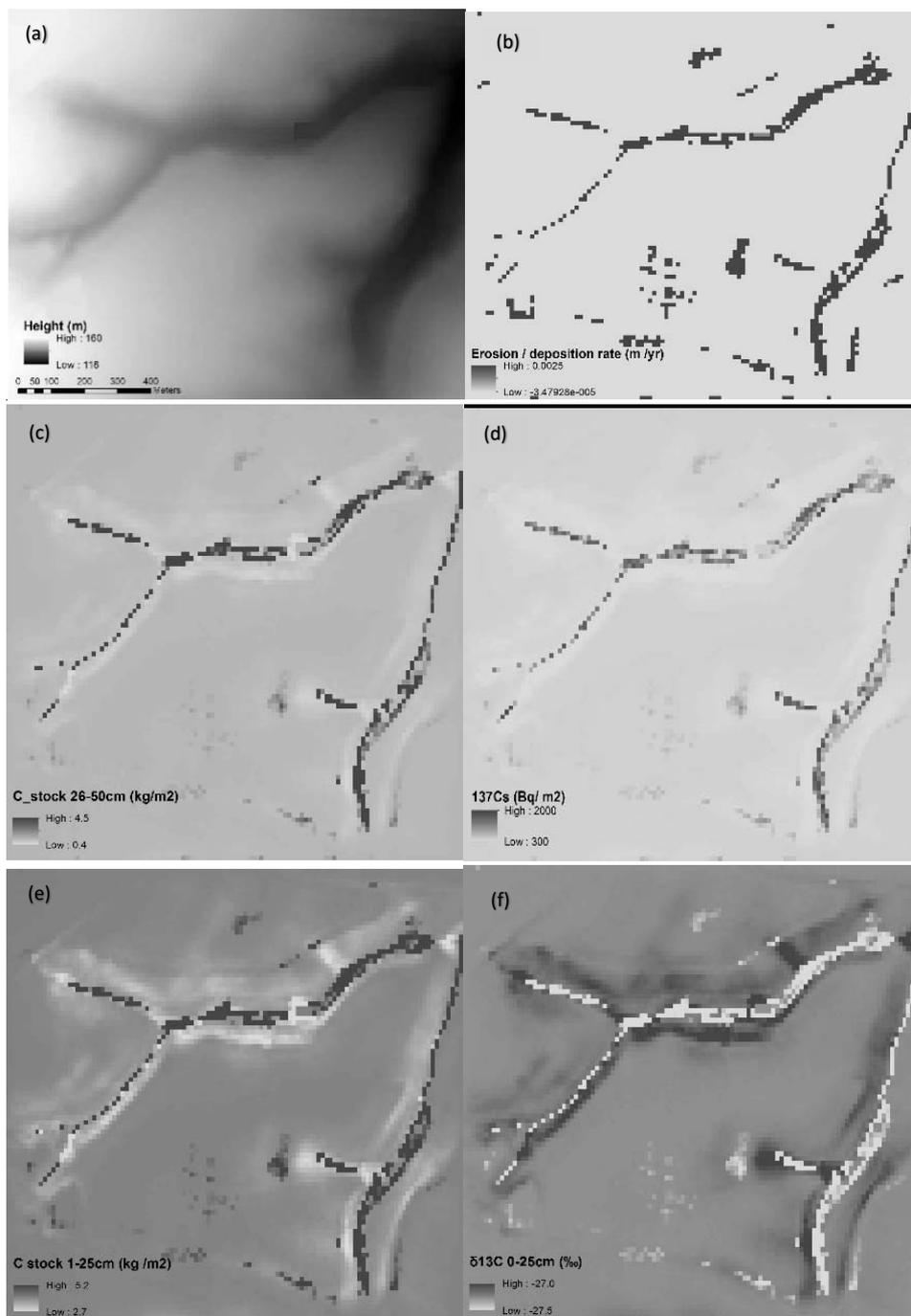
Figure 4: Effects of plant type change and Suess effect on the  $\delta^{13}\text{C}$  profiles.



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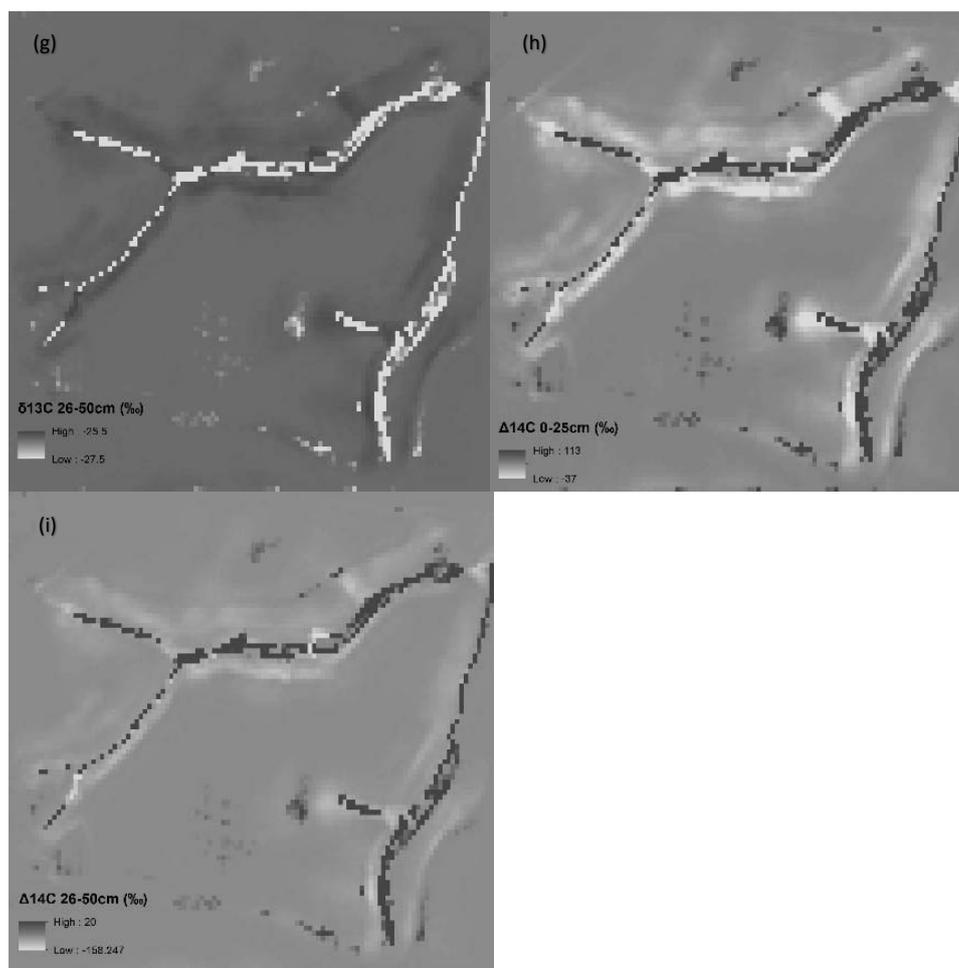
Figure 5: The simulated  $\Delta^{14}\text{C}$  profiles in (a) Scenario 1, (b) Scenario 2, and (c) Scenario 3. See Section 2.7 for the descriptions of scenarios. In b,  $K$  ( $\text{m}^2 \text{yr}^{-1}$ ) is the diffusion coefficient and  $v$  ( $\text{m yr}^{-1}$ ) is the advection term (Eq. 18). In c, the numbers in the legend are the erosion or deposition rates ( $\text{cm yr}^{-1}$ ) with negative values indicating erosion and positive values indicating deposition.

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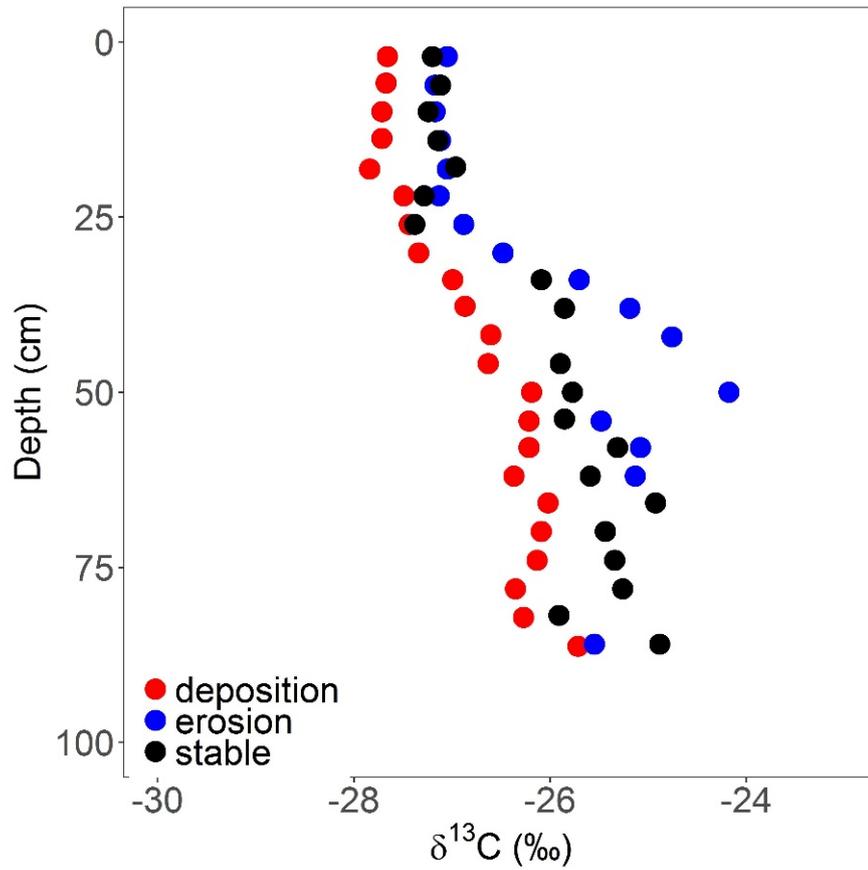


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**Figure 6: Model simulations of erosion and erosion-induced spatial variability of SOC stock and isotopic compositions. (a) DEM (digital elevation model) of the field, (b) erosion and deposition rates (positive values indicate deposition and negative values indicate erosion), (c)  $^{137}\text{Cs}$  inventory, (d) C stock of topsoil (0-25 cm), (e) C stock of subsoil (26-50 cm), (f)  $\delta^{13}\text{C}$  values of topsoil (0-25 cm), (g)  $\delta^{13}\text{C}$  values of subsoil (26-50 cm), (h)  $\Delta^{14}\text{C}$  values of topsoil (0-25 cm), and (i)  $\Delta^{14}\text{C}$  values of subsoil (26-50 cm).**



415 Figure 7: Observed average  $\delta^{13}\text{C}$  profiles of stable, erosion, and depositional areas in a cropland with conventional tillage in Hudenburg, Belgium.

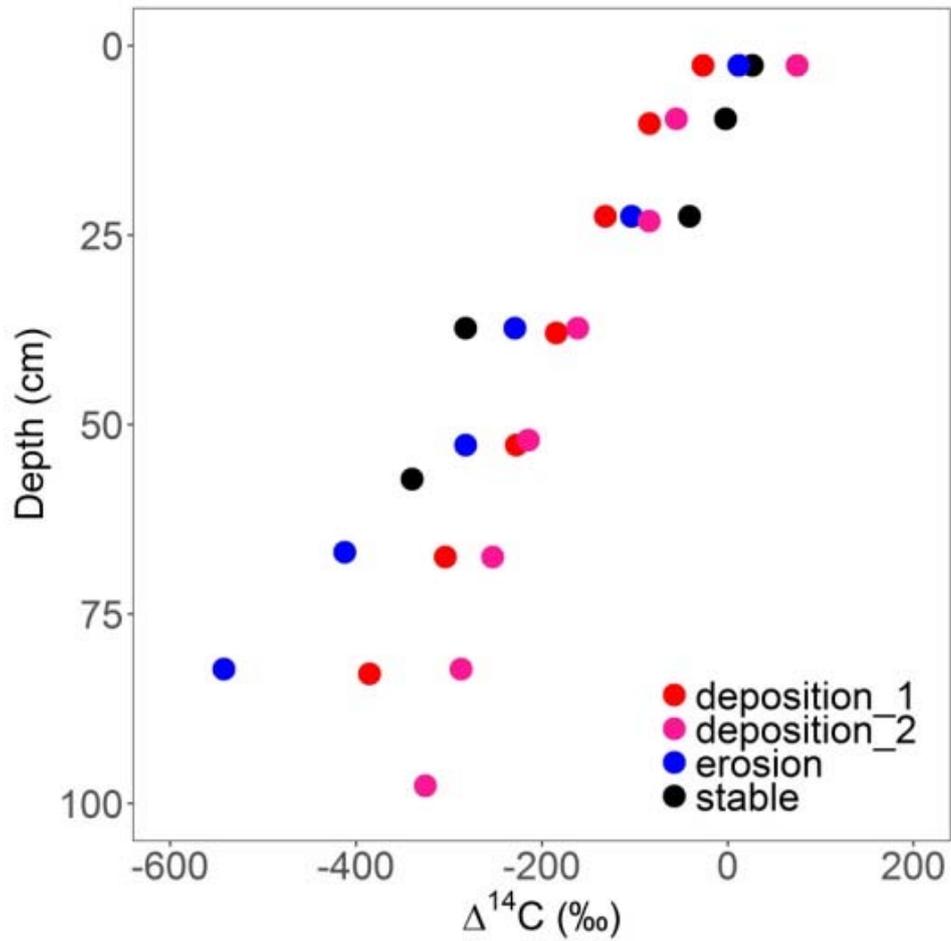


Figure 8: Observed  $\Delta^{14}\text{C}$  profiles in an eroding landscape. This figure is adapted from Berhe et al. (2008).

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